



HRP Investigators Workshop – Feb, 2016



CLOSED LOOP CONTROL COMPACT EXERCISE DEVICE FOR USE ON MPCV

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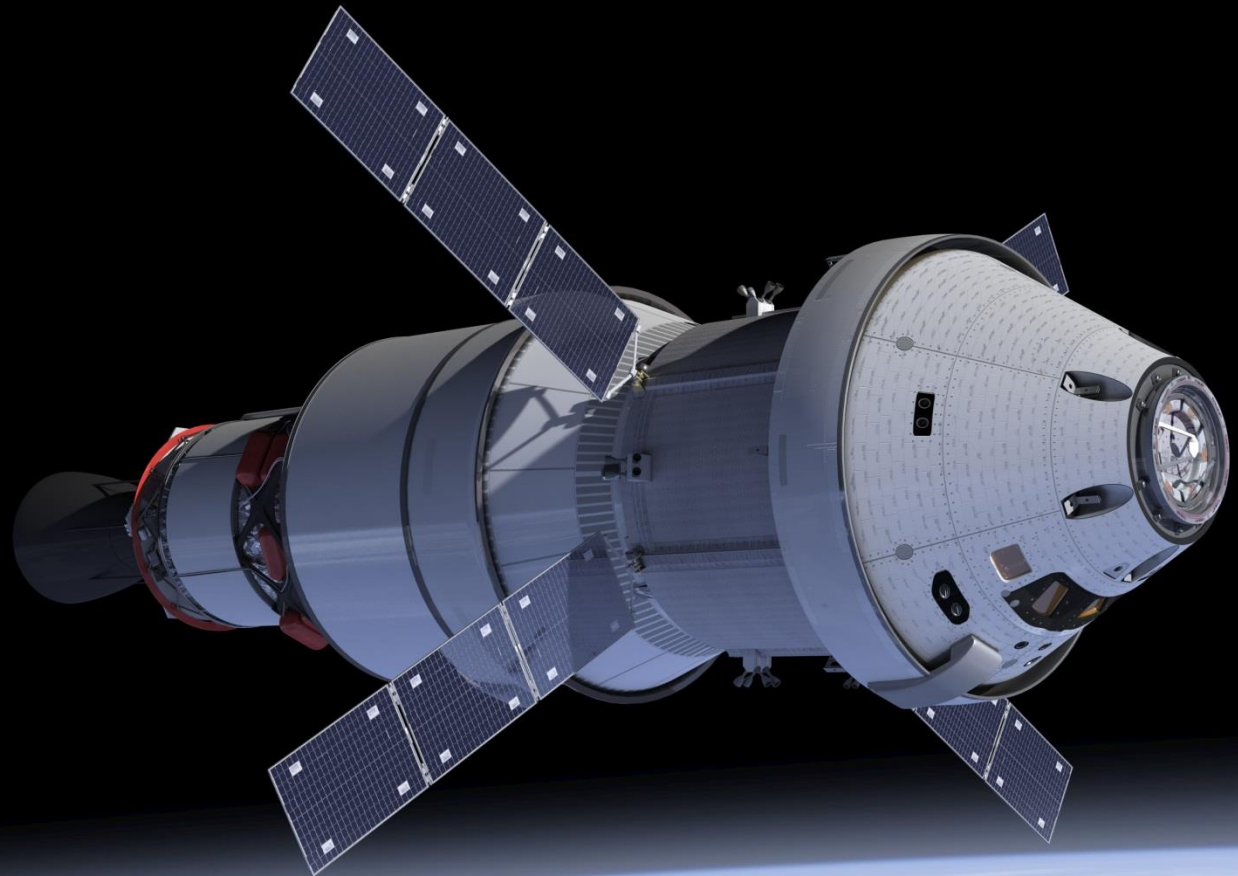
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Motor Driven Exercise Devices



- ❑ AEC-REQ-001 'Exercise Device for Orion EM-2 Functional Requirements'
 - 23.37 lbm
 - 13.5"-21.0" width x 13.5" height x 7.5" depth
 - 480W peak power draw from MPCV
 - Aerobic
 - Provide 450W average aerobic load, 30 min interval
 - Provide 750W peak power load, any interval that conforms to vehicle peak power draw
 - Resistive
 - Provide 400 lb peak load capability
 - Peak linear velocities per figure
- ❑ Motor technology offers
 - Excellent torque density
 - Excellent load accuracy
 - Custom impedance algorithms
 - Custom load versus position

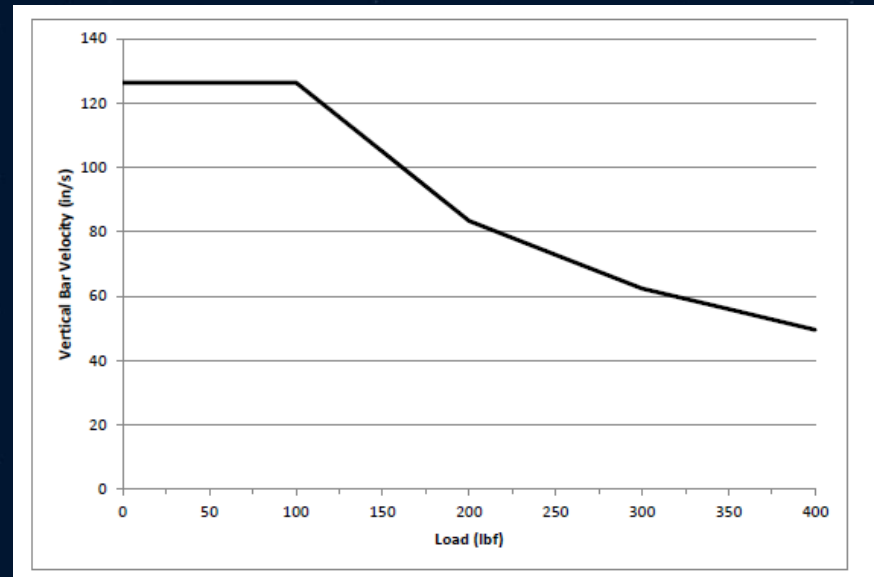


Fig. 1 Linear Velocity (in/s) versus Load Setting



ROCKY

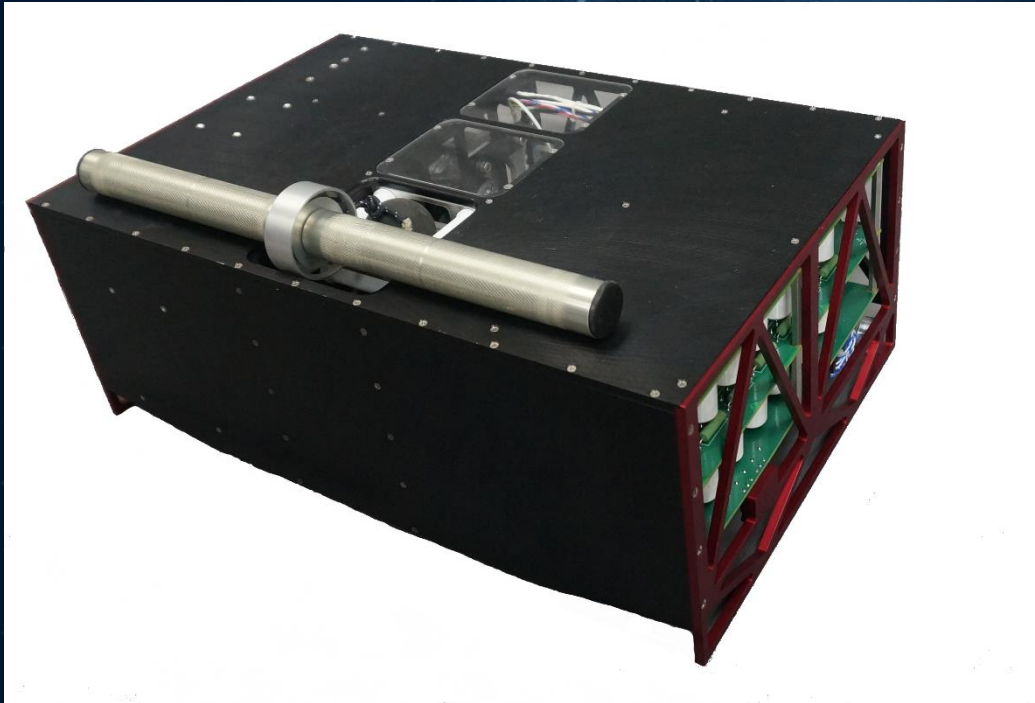


Fig. 2 Resistive Overload Combined with Kinetic Yo-Yo





ROCKY

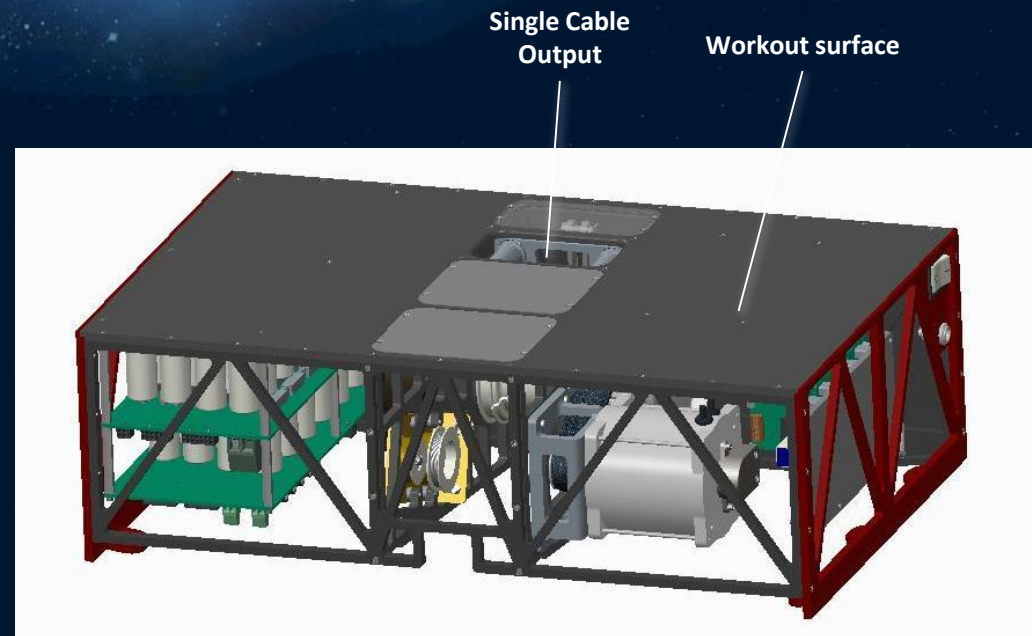
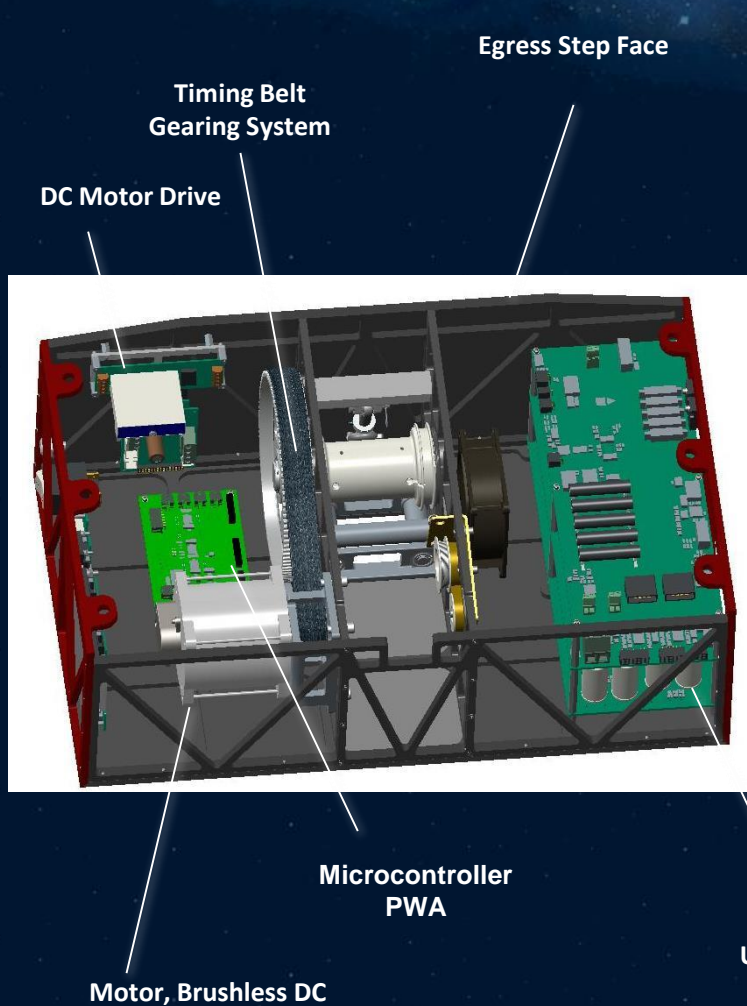


Fig. 3 Resistive Overload Combined with Kinetic Yo-Yo



ROCKY

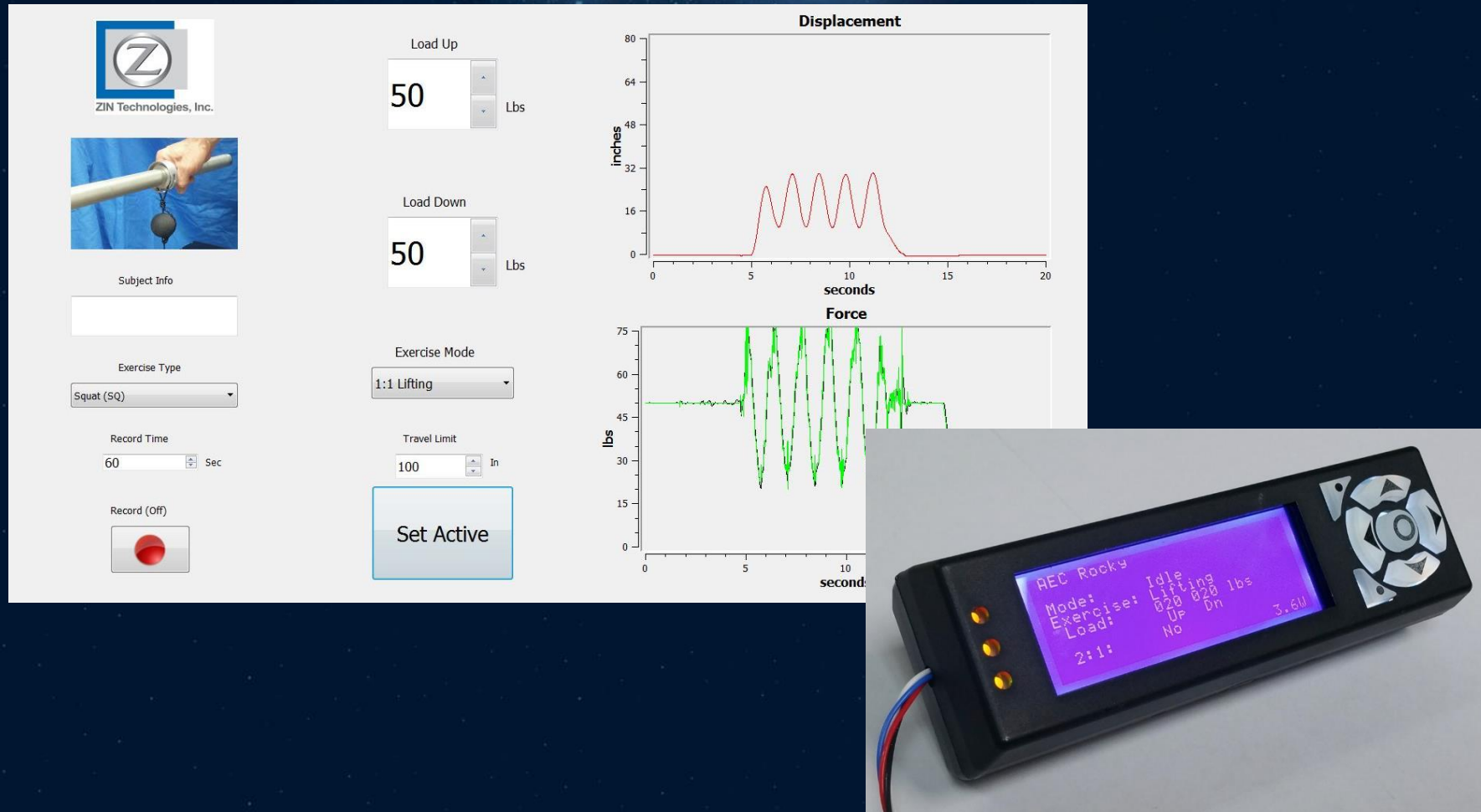


Fig. 4 ROCKY LabVIEW GUI and Standalone Hand Held Display



ROCKY



- **ROCKY is implementing aspects of TDA 'Device for Aerobic and Resistive Training' (DART) which was funded by NASA SBIR**
- **Phase III Tasks include collaboration with ZIN:**
 - Deliver bar with captive pulley (2:1) bar to enable high load and lower velocity exercise
 - Create updated rowing algorithm
 - Create updated load application algorithm
 - Overall assessment of weight reduction on system performance
 - Lessons learned

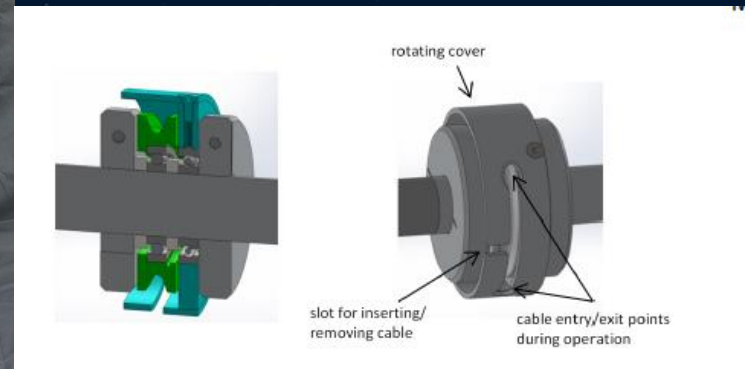
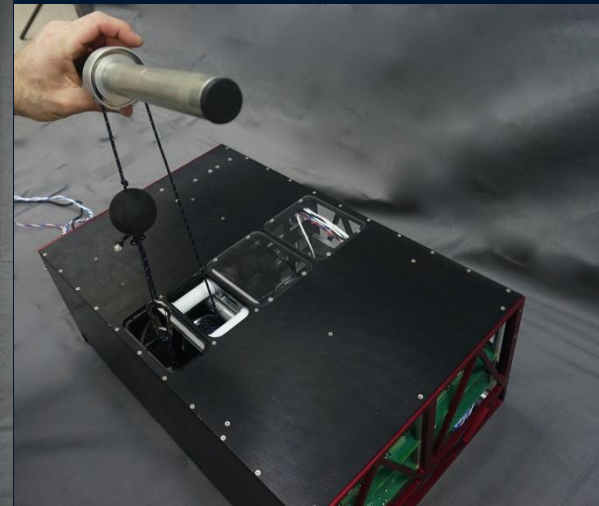


Fig. 5

1:1 and 2:1 Bar Set Ups and Captive Pulley with Rotating Cover



ROCKY

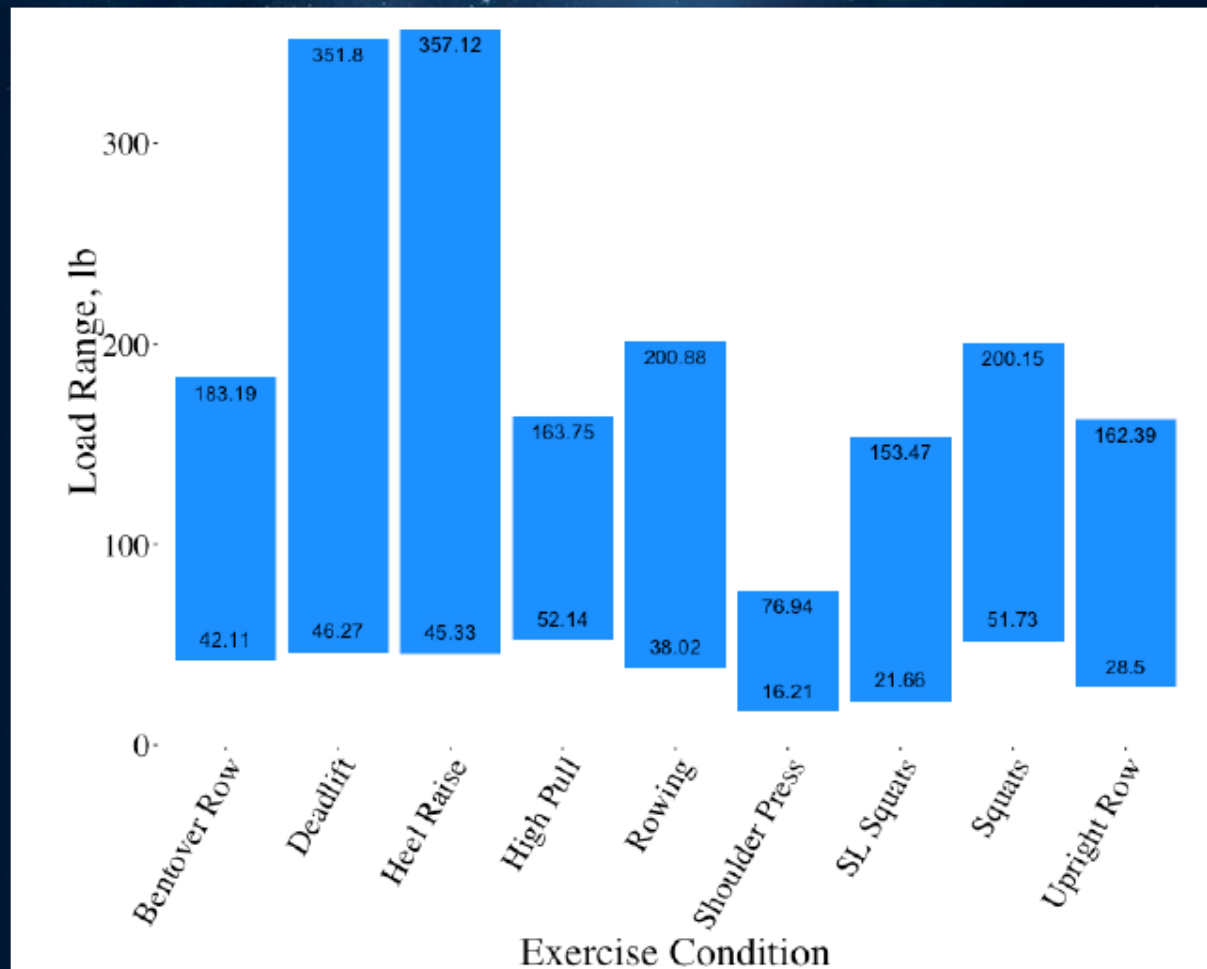


Fig. 6 Load Range versus Exercise Type (data courtesy of JSC Exercise Physiology and Countermeasures Lab – DeWitt and Fincke)

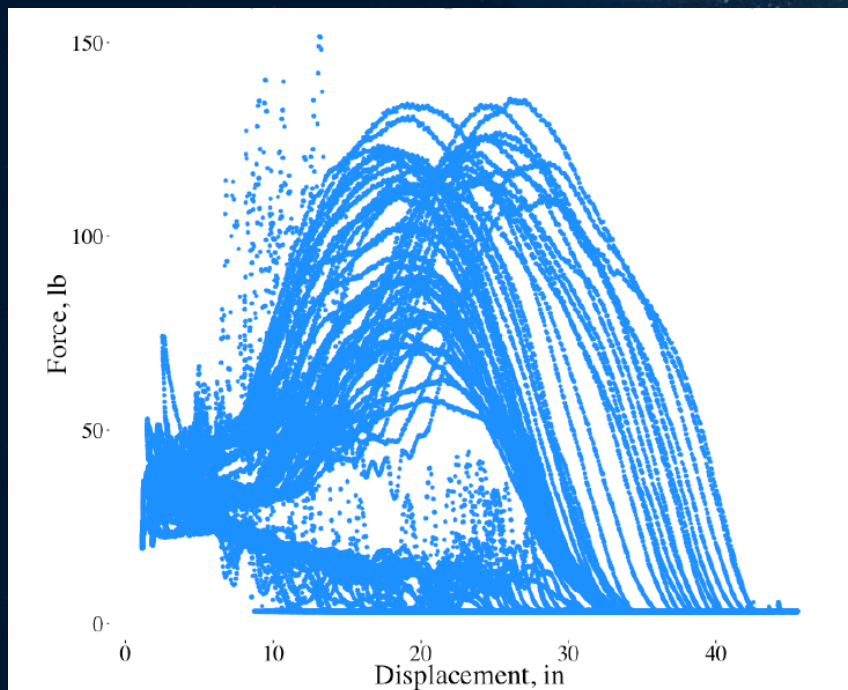


Fig. 7 Force versus Displacement (Rowing)

Device was set at setting #5. The following features were noted:

- Load is maximum in middle of the stroke (peaks between 100-150 lb)
- Very little return load
- Loading is consistent between strokes, although there is variation in stroke length for the subjects

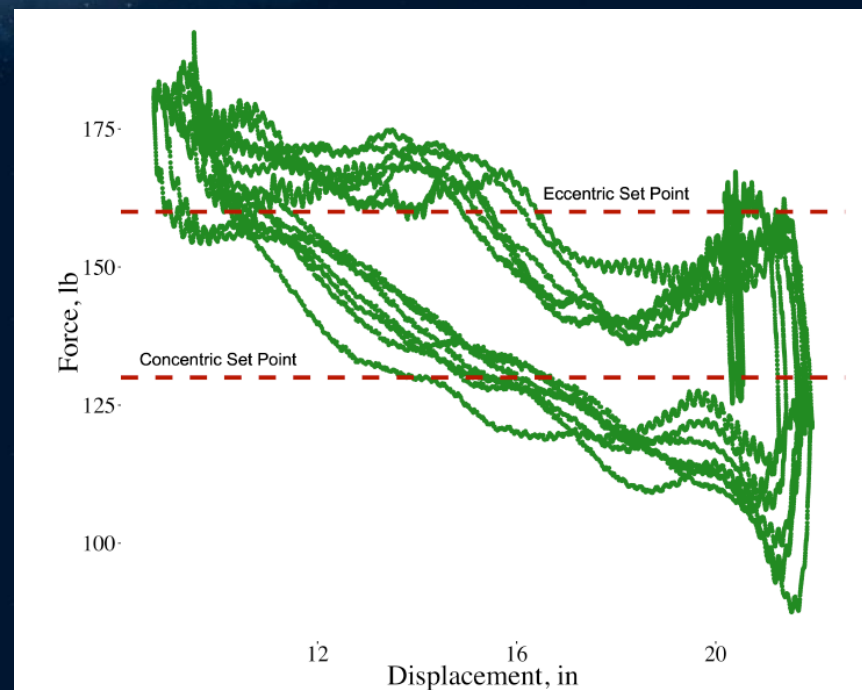


Fig. 8 Force versus Displacement (Squat)

Device was set at 130 lb concentric, 160 lb eccentric. The following features were noted:

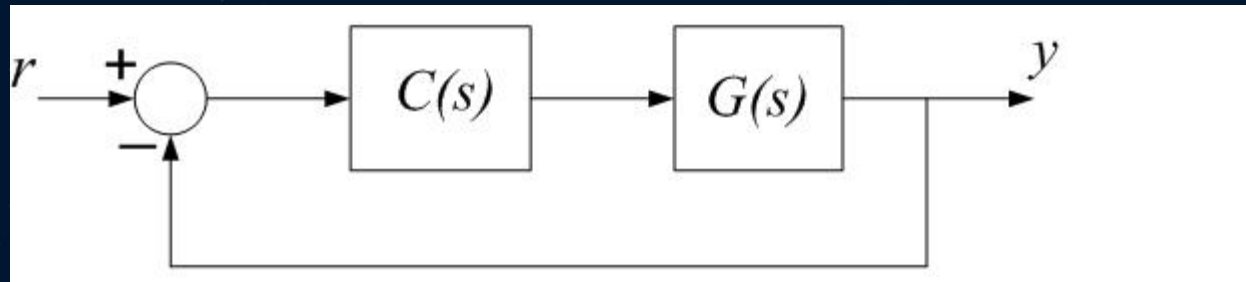
- Load varied throughout completion of the repetition, with a decrease as displacement increased (possibly due to inertia of the bar)
- Sharp change in load at the completion of the upward motion (peak displacement) as eccentric overload initiates



Motor Control Theory



- Open Loop
- Closed Loop
 - Proportional-Integral-Derivative (PID)
 - Linear Quadratic Regulator (LQR)
 - H-Infinity





PID Control

$$u(t) = \underbrace{ke(t)}_{\text{Proportional}} + \underbrace{k_i \int_0^t e(\tau) d\tau}_{\text{Integral}} + \underbrace{k_d \frac{de}{dt}}_{\text{Derivative}}$$

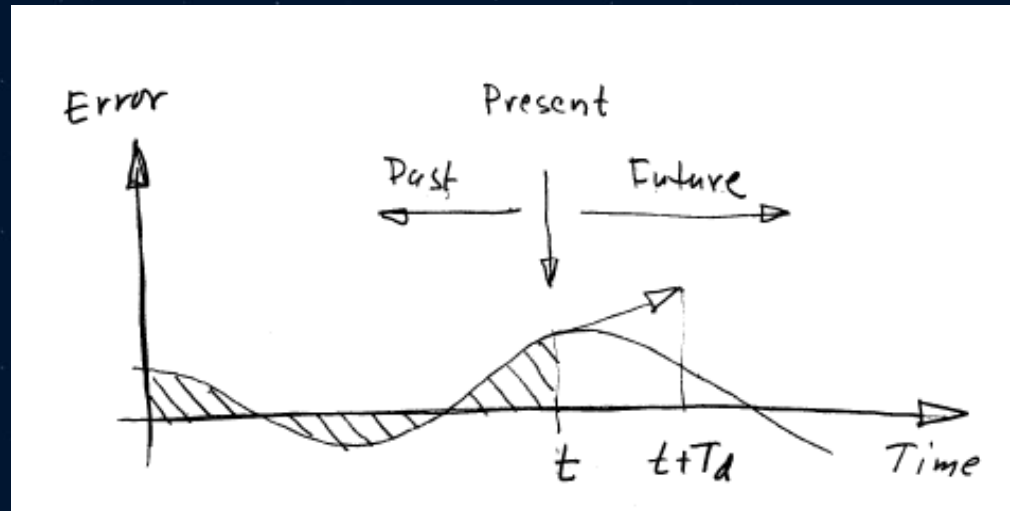


Fig. 9 PID Control



PID Control

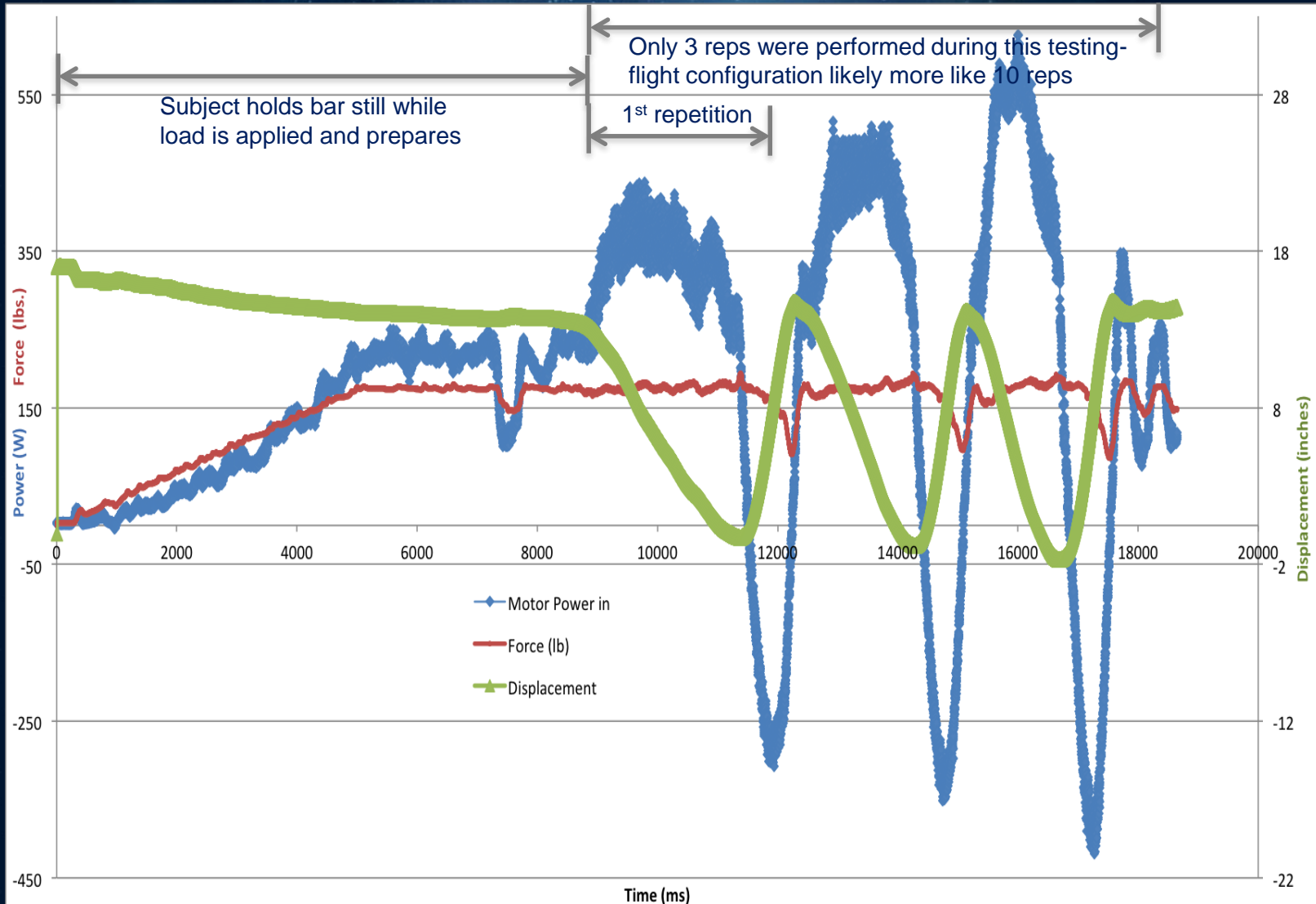


Fig. 10 ROCKY PID Control for Resistive Exercise
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PID Control



- ROCKY Control
 - Aerobic control is PID around a velocity set point

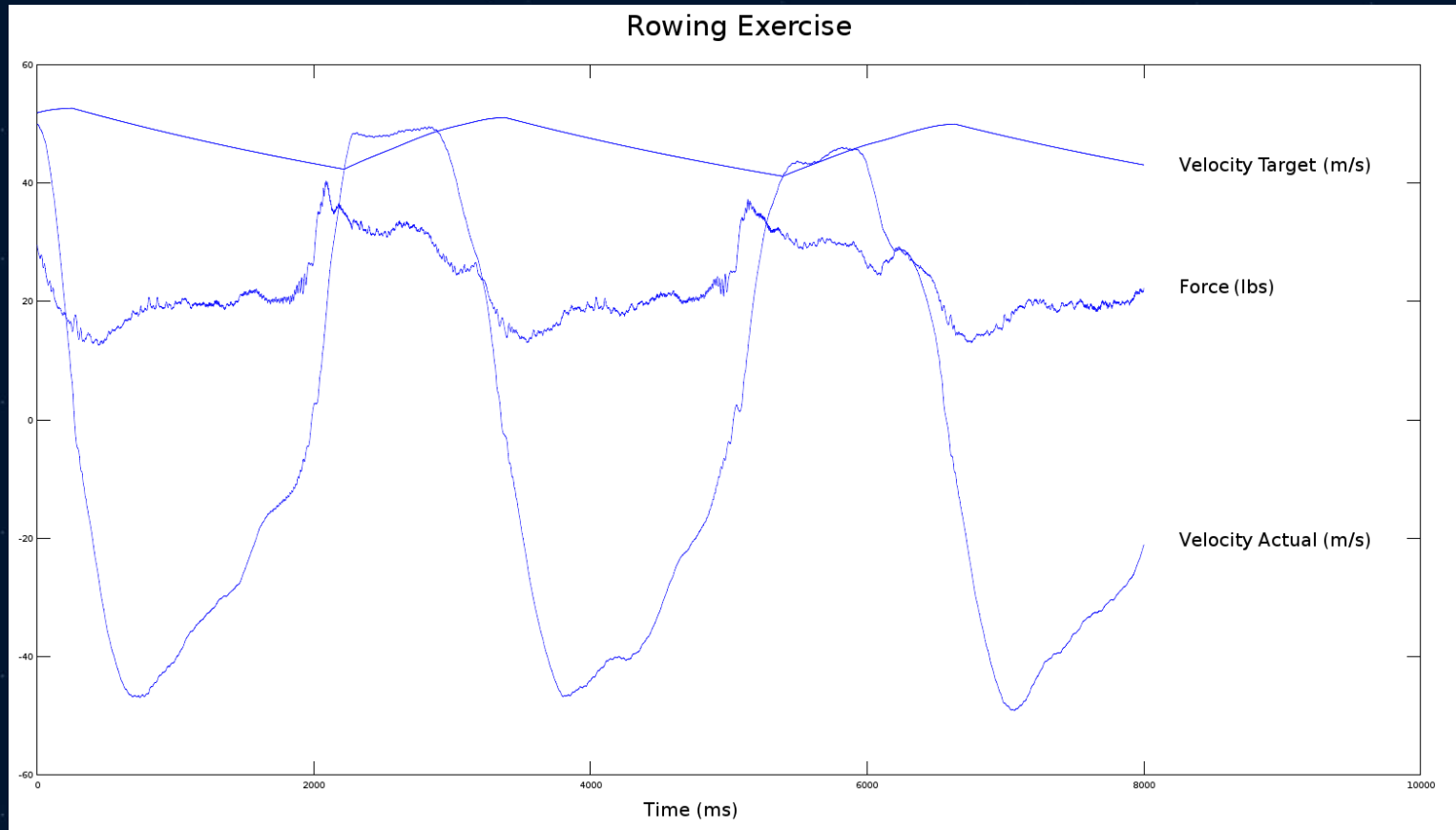


Fig. 11 ROCKY PID Control for Aerobic Exercise



LQR Control

- Classical optimal control theory has evolved over time to formulate LQRs which minimizes the excursion in state trajectories of a system while requiring minimum controller effort
 - The optimal quadratic regulator design is a reduction of the Algebraic Riccati Equation and is used to calculate state feedback gains for a chosen set of weighting matrices
 - These weighting matrices regulate the penalties on the deviation in trajectories of the state variables and control signal
 - Using a model to synthesize all internal states

$$\dot{x} = Ax + Bu \quad \text{Given system}$$

$$u = Fx \quad \text{State feedback control to stabilize the system}$$

$$J = \int_0^{\infty} [x^T(t)Qx(t) + u^T(t)Ru(t)]dt$$

Defined cost functional performance index

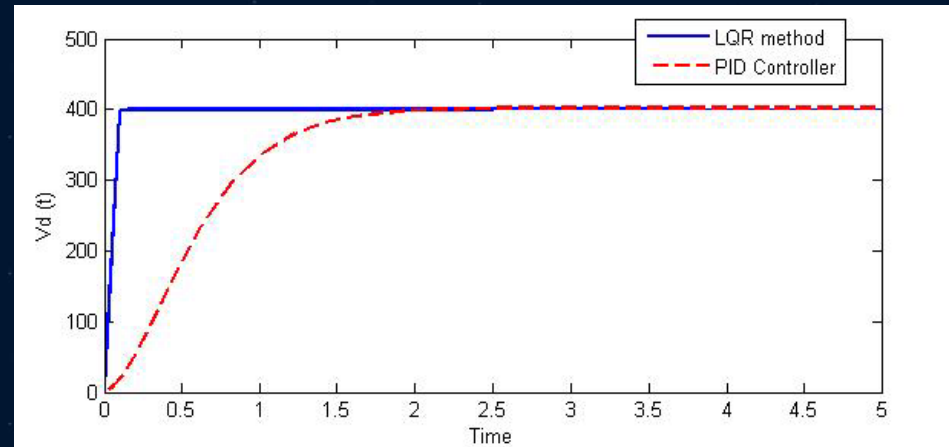


Fig 12 Highly Generalized Comparison of PID v. LQR Control Methods



H Infinity Control

- H_∞ control synthesis:
 - High disturbance rejection
 - High stability
 - High order controllers (complex and resource intensive)
- This controller design is generally based on minimization of a function (H_∞ norm of selected closed loop system)

Lower fractional transformation

$$\|F_1(M, K)_\infty = \sup \underbrace{\bar{\sigma}}_{\text{Singular value of } F(M,K)}(\underbrace{F_1(M, K)(j\omega)}_{\text{Lower fractional transformation}})$$

Singular value of $F(M,K)$

Other Methods

- Semi-active Impedance Modulation with Ultracapacitors (H. Richter, A. van den Bogert, D. Simon)
 - Electromechanical system which can be programmed to produce any desired mechanical impedance
 - Dynamic relationship between force and velocity at the user is called impedance
 - Bungees = 'stiffness' impedance
 - Rowing = 'inertial' impedance
 - Energy regeneration and storage
 - Designed a small (100N, 0.5m/s capability) hand operated system which is:
 - Power neutral (excepting for small microprocessor batteries)
 - Highly configurable – the impedance perceived by the user can be arbitrarily defined and is enforced by the control system

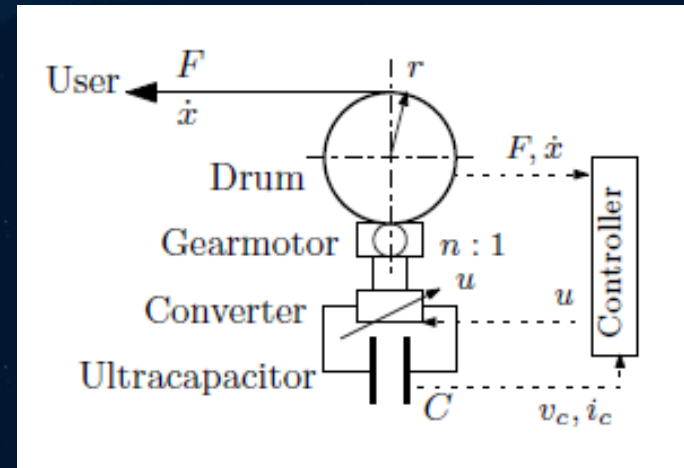


Fig 14. Advanced Rowing Ergometer Concept to Demonstrate Feasibility of Semi-Active Modulation to Match Commercial Ergometer F-V Characteristics



References



- Caltech Control & Dynamical Systems Class Notes (Chapter 8, PID Control), 2004
- 'Comparison Performance Between PID and LQR Controllers for 4-leg Voltage Source Inverters', A. Mohammadbagheri, N. Zaeri, M. Yaghoobi, 2011
- 'H-Infinity Controller Design for a DC Motor Model with Uncertain Parameters', L. Brezina, T. Brezina, 2011
- 'Application of Multivariable Techniques to Design Experimentally a Flexible Satellite Attitude Control System', J. de Castro, L. de Souza, 2010
- 'Plant and Control Design for Advanced Exercise Machines with Energy Regeneration', H. Richter, 2015